

(11) **EP 1 391 442 B1**

(12)

EUROPEAN PATENT SPECIFICATION

(45) Date of publication and mention of the grant of the patent: 28.04.2010 Bulletin 2010/17

(21) Application number: 01980904.5

(22) Date of filing: 25.10.2001

(51) Int Cl.: **C04B** 35/80 (2006.01)

(86) International application number: PCT/JP2001/009365

(87) International publication number: WO 2002/098819 (12.12.2002 Gazette 2002/50)

(54) METHOD FOR PRODUCING SIC FIBER− REINFORCED SIC COMPOSITE MATERIAL

VERFAHREN ZUR HERSTELLUNG VON MIT SIC-FASERN VERSTÄRKTEM SIC-VERBUNDWERKSTOFF

PROCEDE DE PRODUCTION D'UN MATERIAU COMPOSITE AU CARBURE DE SILICIUM SIC RENFORCE DE FIBRES SIC

(84) Designated Contracting States: **DE FR GB IT SE**

(30) Priority: 31.05.2001 JP 2001164996

(43) Date of publication of application: **25.02.2004 Bulletin 2004/09**

(73) Proprietor: Japan Science And Technology Agency Kawaguchi-shi Saitama 332-0012 (JP)

(72) Inventors:

 KOHYAMA, Akira c/o Institute of Advanced Energy Uji-shi, Kyoto 611-0011 (JP)

 KATOH, Yutai c/o Institute of Advanced Energy Uji-shi, Kyoto 611-0011 (JP)

(74) Representative: Müller-Boré & Partner Patentanwälte
Grafinger Strasse 2
81671 München (DE)

(56) References cited:

- YANO T ET AL: "TEM investigation and fracture behavior of SiC/SiC composites fabricated by hot-pressing" KEY ENGINEERING MATERIALS TRANS TECH PUBLICATIONS SWITZERLAND, vol. 166, 1999, pages 135-138, XP008061768 ISSN: 1013-9826
- PATENT ABSTRACTS OF JAPAN vol. 1999, no. 10, 31 August 1999 (1999-08-31) & JP 11 130552
 A (JAPAN ATOM ENERGY RES INST), 18 May 1999 (1999-05-18)
- YOSHIDAKETAL: "Room and High-Temperature Mechanical and Thermal Properties of SiC Fiber-Reinforced SiC Composite Sintered Under Pressure" JOURNAL OF NUCLEAR MATERIALS, AMSTERDAM, NL, vol. 283-287, 2000, pages 560-564, XP002313461 ISSN: 0022-3115

P 1 391 442 B1

Note: Within nine months of the publication of the mention of the grant of the European patent in the European Patent Bulletin, any person may give notice to the European Patent Office of opposition to that patent, in accordance with the Implementing Regulations. Notice of opposition shall not be deemed to have been filed until the opposition fee has been paid. (Art. 99(1) European Patent Convention).

Description

20

30

40

45

50

55

[0001] The present invention relates to a method of manufacturing a SiC fiber-reinforced SiC-matrix composite useful as structural members of aircraft, spacecraft, nuclear reactors, nuclear fusion reactors or the like, which are exposed to a high-temperature atmosphere or driven under heavy-duty conditions.

[0002] Various ceramics such as SiC and $\mathrm{Si}_3\mathrm{N}_4$, which have good properties such as heat-resistance, chemical stability and mechanical strength, have been proposed so far for structural members for aircraft, spacecraft, nuclear reactors, nuclear fusion reactors, power plants which consume fossil fuel, or the like exposed to a severe atmosphere under heavy-duty conditions. Such ceramics are also used as members of heat exchangers or mechanical seals driven under heavy-duty conditions. Especially, SiC is a suitable material in various industrial fields from aerospace to nuclear power generation, due to its excellent heat-, corrosion- and wear-resistance as well as chemical stability and mechanical strength.

[0003] SiC is brittle itself, despite of good high-temperature property with a sublimation temperature higher than 2600°C. In order to overcome poor toughness, a SiC fiber-reinforced SiC-matrixcomposite (hereinafter referred to as merely "a SiC composite") has been proposed, as reported in A. Lacombe and C. Bonnet, 2nd Int. Aerospace Planes Conf. Proc. AIAA-90-5208 (1990) and C. W. Hollenberg et al., J. Nucl. Mat., 219, (1995)70-86.

[0004] Several methods, e.g. hot-pressing and liquid-phase sintering, have been developed so far for manufacturing a SiC composite. However, since it is very difficult to manufacture a SiC composite having high mechanical strength and excellent rupture property, the same steps are necessarily repeated in order to improve properties of the SiC composite. Repetition of the same steps complicates a manufacturing process and raises a manufacturing cost. Moreover, members with complicated profiles can not be manufactured with ease due to repetition of the same steps. In this meaning, a SiC composite has not been available for industrial application, yet.

[0005] By the way, a liquid-phase sintering method has been proposed, whereby heat-resistant SiC fiber, which has quasi-stoichiometric composition with high crystallinity, is used for reinforcement and a matrix of a SiC composite is formed by liquid-phase sintering. The manufactured SiC composite has a dense structure with excellent thermal conductivity. However, there still remain unsolved problems for well-balancing rupture strength with toughness at high levels. **[0006]** Key Engineering Materials Vol. 166 (1999), pages 135-138, discloses the fabrication of continuous SiC fiber-reinforced SiC composite by hot pressing at 1650°C or 1750°C using Al-B-C or Al₂O₃-Y₂O₃-CaO sintering additives. JP-11-130552 discloses a method for producing a ceramic reinforcing fiber/ceramic matrix composite material by impregnating a silicon carbide fiber woven fabric or silicon staple fibers as reinforcing fibers with a polycarbosilane, a cyclic polysilazane and/or a polyvinyl silane.

[0007] An object of the present invention is to manufacture a SiC composite, which has a dense structure with high strength, by one-step hot-pressing. Formation of the dense structure is realized by use of SiC fiber coated with carbon, boron nitride or silicon carbide.

[0008] According to the present invention, a slurry is prepared by suspension of fine SiC powder and a sintering additive in silicone polymer. A preform of SiC fiber, which is coated with one or more of carbon, boron nitride and silicon carbide, is impregnated with the slurry. The impregnated preform (i.e. a prepreg) is then hot-pressed.

[0009] The sintering additive is one or more selected from Al₂O₃, Y₂O₃, SiO₂ and CaO. The slurry further contains a silicone polymer such as polycarbosilane, polyvinylsilane and polymethylsilane.

[0010] When the prepreg, which is prepared by impregnation of a SiC fiber preform with the slurry, is hot-pressed at 1600-1800°C with a pressure of 10 MPa or more, it is liquid-phase sintered to a dense and tough SiC composite.

Fig. 1 is a microscopic view of several SiC composites for explaining an effect of a carbon coating on reaction between SiC fiber and a matrix.

Fig. 2 is a graph showing stress-strain curves of several SiC composites for explaining remarkable improvement of strength of a SiC composite due to C-coated SiC fiber.

[0011] SiC fiber, for reinforcement of SiC composite exposed to extreme environments, necessarily has quasi-stoi-chiometric composition, which controls impurities such as oxygen at lowest possible levels, with high crystallinity. However, the SiC fiber is often degraded or damaged by reaction with a matrix during sintering a prepreg of SiC fiber mixed with fine SiC powder. The reaction of SiC fiber with the matrix can be inhibited by coating the SiC fiber with one or more of carbon, boron nitride and/or silicon carbide according to the present invention.

[0012] The C, BN and/or SiC coating suppresses mutual diffusion between a matrix and SiC fiber and prevents SiC fiber from being damaged. The coating also advantageously controls rupture strength of SiC composite, since dispersion or discontinuation of cracks and pull-out of SiC filaments are promoted by the coating during collapse of the SiC composite. As a result, a SiC fiber preform impregnated with a slurry can be hot-pressed with a high pressure enough to densify the SiC composite.

[0013] A slurry for impregnation of a SiC fiber preform comprises fine SiC powder as a component for formation of a

matrix and one or more sintering additives of Al_2O_3 , Y_2O_3 , SiO_2 and CaO. The sintering additive and SiC powder are converted to a transient liquid phase at 1800 °C or lower, resulting in promotion of sintering reaction and densification of a SiC composite.

[0014] The slurry further contains a silicone polymer such as polycarbosilane, polyvinylsilane and polymethylsilane. Although particles in the slurry are hardly fed into fine cavities between SiC filaments, the silicone polymer infiltrates into the fine cavities and raises density of a manufactured SiC composite.

[0015] A SiC fiber preform impregnated with a slurry was hot-pressed to a SiC composite. A sintering temperature and a pressure are preferably determined within ranges of 1600-1800°C and 10 MPa or more, respectively. A manufactured SiC composite is more densified as elevation of a sintering temperature and increase of an applied pressure. However, the sintering temperature shall be limited to 1800°C at highest; otherwise SiC fiber would be significantly damaged even with a pressure of 10 MPa or so. SiC fiber is also damaged at an overpressure above 30 MPa. Damage of SiC fiber leads to decrease of mechanical strength of a product. On the other hand, a matrix is insufficiently sintered with many cavities in a sintered body at a heating temperature lower than 1600°C. As a result, a product does not have properties suitable for the purpose. A pressure below 10 MPa is insufficient for reduction of cavities in a sintered body even at a sintering temperature of 1800°C or so.

[0016] The other features of the present invention will be clearly understood from the following Example, referring to the drawings.

[0017] SiC fiber (offered as Tyranno[™]-SA by Ube Industries, Ltd.), which had quasi-stoichiometric composition with high crystallinity, was used as strengthening fiber. A C or BN coating of approximately 1 μ m in thickness was formed on surfaces of SiC filaments by CVD process for vapor-depositing pyrolyzed carbon or boron nitride on the SiC filaments. **[0018]** A slurry for impregnation of SiC fiber was prepared by dispersing fine β -SiC powder, Al₂O₃ (a sintering additive) of 0.3 μ m in average particle size and polycarbosilane at a mass ratio of 4.5 : 0.5 : 5 in hexane (a solvent). A SiC fiber preform was impregnated with the slurry at a mass ratio of SiC fiber to the matrix-forming material being 4 : 6 by vacuum evacuation.

[0019] Several impregnated SiC fiber preforms (prepregs) were individually set in a hot-pressing machine and hot-pressed under conditions shown in Table 1. Properties of manufactured SiC composites are also shown in Table 1.

			•			
Sample No.	1	2	3	4	5	6
Coating SiC fiber with	no	С	С	С	BN	BN
thickness (μm)	-	1	1	1	1	1
A sintering temperature (°C)	1750	1720	1750	1750	1750	1750
A pressure (MPa)	15	20	15	15	20	15
Particle size of β-SiC (nm)	20	20	20	270	20	20
Density (mg/m ³)	2.9	2.8	2.8	2.7	2.9	2.8
Flexural strength (MPa)	251	559	628	438	603	588
Flexural elasticity (GPa)	242	160	181	131	239	185
Flexural fracture energy (MJ/m ²)	0.43	9.3	7.0	2.7	4.8	7.9

Table 1: Conditions of Hot-Pressing and Properties of SiC Composite

[0020] A SiC composite, which was manufactured by hot-pressing a prepreg of SiC fiber coated with C or BN at 1750°C with a pressure of 15 MPa, had flexural strength and flexural fracture energy remarkably higher than a SiC composite Sample No. 1 manufactured from a prepreg of non-coated SiC fiber.

[0021] A structure of each SiC composite was observed by a scanning electron microscope (SEM) in order to research an effect of coatings on flexural properties. Results are shown in Fig. 1. As noted in the SiC composite Sample No. 1 using un-coated SiC fiber, the SiC fiber was heavily damaged due to its reaction with a matrix. On the other hand, the SiC composites Sample Nos. 2-4 maintained integrity of the SiC fiber due to C coatings, which completely inhibited reaction of the SiC fiber with a matrix. However, some cavities were detected in the matrix of the SiC composite Sample No. 4 without infiltration of β -SiC particles into gaps between SiC filaments, since the β -SiC particles were relatively big in size.

[0022] Each of Sample Nos. 1-4 was subjected to a three point-bending test for researching a stress-strain curve as shown in Fig. 2. It is apparently noted from comparison with the SiC composite Sample No. 1 that any of the SiC composites using C-coated SiC fiber had maximum load above its elastic limit and elongation after the maximum load. The results suggest that quasi-ductile fracture behavior was imparted to the SiC composite by the C coating.

30

20

35

40

50

55

[0023] Figs. 1 and 2 show the effects of C-coatings, but the same effects were also gained in case of hot-pressing a prepreg of BN-coated SiC fiber without reaction of the SiC fiber with a matrix. The resultant SiC composite had high mechanical strength.

[0024] According to the present invention as above-mentioned, SiC fiber for use as reinforcement is coated with C, BN or the like to prevent SiC fiber from being damaged during sintering. As a result, a sintered body can be manufactured without degradation of inherent properties of a SiC fiber-reinforced SiC-matrix composite. Prevention of the SiC fiber from being damaged enables elevation of a sintering temperature and increase of a pressure during hot-pressing for further improvement of properties of the SiC composite. Consequently, the manufactured SiC composite is useful as structural members for aircraft, spacecraft, atomic reactors, atomic fusion reactors, power generating plants driven under heavy-duty conditions and so on.

Claims

10

15

20

25

30

35

40

50

55

1. A method of manufacturing a SiC fiber-reinforced SiC-matrix composite, which comprises the steps of:

preparing a slurry, which disperses fine SiC powder and a sintering additive in a silicone polymer; impregnating a preform of SiC fiber, which is coated with one or more of carbon, boron nitride and silicon carbide, with said slurry; and

hot-pressing said impregnated preform,

wherein the sintering additive is one or more of Al₂O₃, Y₂O₃, SiO₂ and CaO.

- 2. The manufacturing method defined by Claim 1, wherein the slurry further contains one or more silicone polymers selected from polycarbosilane, polyvinylsilane and polymethylsilane.
- 3. The manufacturing method defined by Claiml, wherein the impregnated preform is hot-pressed at 1600-1800°C with a pressure of 10 MPa or more.

Patentansprüche

1. Verfahren zur Herstellung eines SiC-Faser-verstärkten SiC-Matrix-Verbundstoffes, umfassend die Schritte:

das Herstellen einer Aufschlämmung, welche feines SiC-Pulver und ein Sinteradditiv in einem Siliconpolymer dispergiert;

das Imprägnieren einer Vorform einer SiC-Faser, welche mit einem oder mehreren von Kohlenstoff, Bornitrid und Siliciumcarbid beschichtet ist, mit der Aufschlämmung; und

das Heißpressen der imprägnierten Vorform,

wobei das Sinteradditiv eines oder mehrere von Al₂O₃, Y₂O₃, SiO₂ und CaO ist.

- 2. Herstellungsverfahren nach Anspruch 1, wobei die Aufschlämmung weiter ein oder mehrere Siliconpolymere, ausgewählt aus Polycarbosilan, Polyvinylsilan und Polymethylsilan, enthält.
- **3.** Herstellungsverfahren nach Anspruch 1, wobei die imprägnierte Vorform bei 1600-1800°C mit einem Druck von 10 MPa oder mehr heißgepreßt wird.

Revendications

1. Procédé de fabrication d'un composé à matrice de carbure de silicium (SiC) renforcée de fibres SiC, qui comprend les étapes qui consistent :

à préparer une suspension épaisse qui met en dispersion une fine poudre de SiC et un additif de frittage dans un polymère de silicone ;

à imprégner une préforme de fibre SiC, revêtue d'un ou plusieurs éléments parmi le carbone, le nitrure de bore et le carbure de silicium, de ladite suspension épaisse ; et

à presser à chaud ladite préforme imprégnée,

2. Procédé de fabrication selon la revendication 1, dans lequel la suspension épaisse contient en outre un ou plusieurs

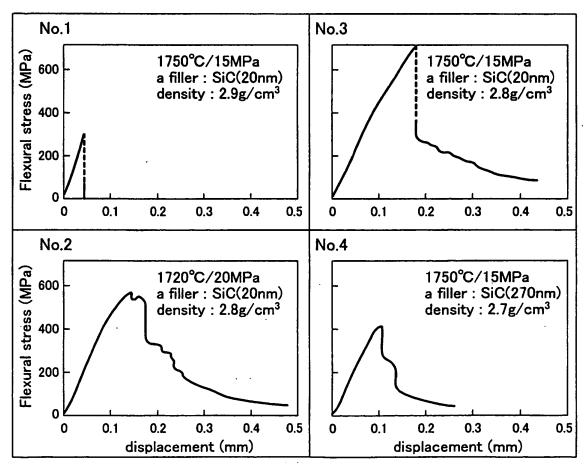
dans lequel l'additif de frittage est un ou plusieurs éléments parmi ${\rm Al_2O_3},\,{\rm Y_2O_3},\,{\rm SiO_2}$ et Cao.

polymères de silicone choisis parmi le polycarbosilane, le polyvinylsilane et le polyméthylsilane.

5	3.	Procédé de fabrication selon la revendication 1, dans lequel la préforme imprégnée est pressée à chaud à une température de 1600 à 1800°C et à une pression supérieure ou égale à 10 MPa.
10		
15		
20		
25		
30		
35		
40		
45		
50		
55		

No.1
No.2
No.2

FIG.2



REFERENCES CITED IN THE DESCRIPTION

This list of references cited by the applicant is for the reader's convenience only. It does not form part of the European patent document. Even though great care has been taken in compiling the references, errors or omissions cannot be excluded and the EPO disclaims all liability in this regard.

Patent documents cited in the description

JP 11130552 A [0006]

Non-patent literature cited in the description

- A. Lacombe; C. Bonnet. 2nd Int. Aerospace Planes Conf. Proc. AIAA-90-5208, 1990 [0003]
- **C. W. Hollenberg et al.** *J. Nucl. Mat.*, 1995, vol. 219, 70-86 **[0003]**
- Key Engineering Materials, 1999, vol. 166, 135-138[0006]