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Komiyama et al.

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(54) **INFRARED FOCUSING DEVICE** 5,939,709 A * 8/1999 Ghislain et al. 250/216

(75) Inventors: **Susumu Komiyama**, Tokyo (JP); **Kenji Ikushima**, Kanagawa (JP)

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(73) Assignee: **Japan Science and Technology Agency**, Saitama (JP)

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Primary Examiner—Stephone B. Allen
Assistant Examiner—Lee Fineman
(74) *Attorney, Agent, or Firm*—Westerman, Hattori, Daniels & Adrian, LLP.

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(57) **ABSTRACT**

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An infrared light condensing apparatus that focuses an infrared light of several tens microns in wavelength at a microfine area of submicron or less and also a near-field from a microfine area of submicron or less, and permits a scanning image to be obtained. It includes a solid immersion lens including a medium of high index of refraction for coupling an incident light or an outgoing light to an antenna, a measured specimen disposed on a base plane of the solid immersion lens, an antenna disposed away from the base plane at a distance 1/4 of an effective wavelength of the light for causing the light to geometrically resonate therewith, a rod-like conductive probe having a sharply point end projecting from the antenna, and a position control means such as a triaxial XYZ mechanical stage for controlling the position of the probe with the intermediary of a cantilever.

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G02B 13/14 (2006.01)

(52) **U.S. Cl.** **359/350; 359/356**

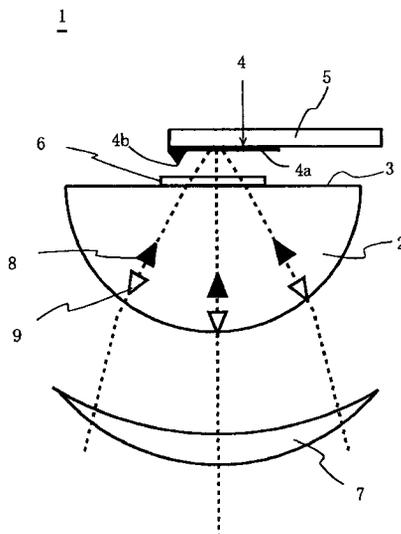
(58) **Field of Classification Search** None
See application file for complete search history.

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9 Claims, 10 Drawing Sheets



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FIG. 1

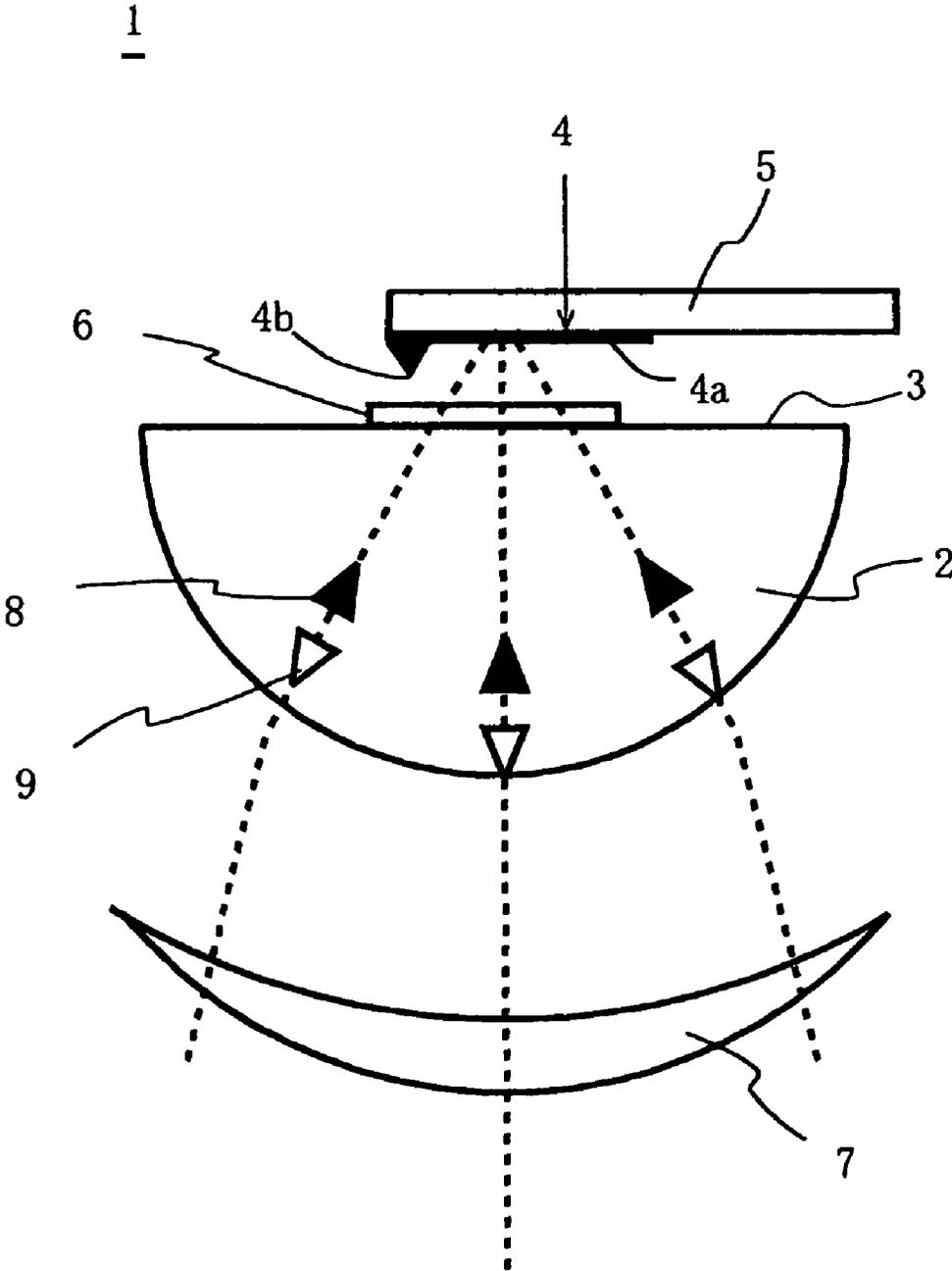


FIG. 2

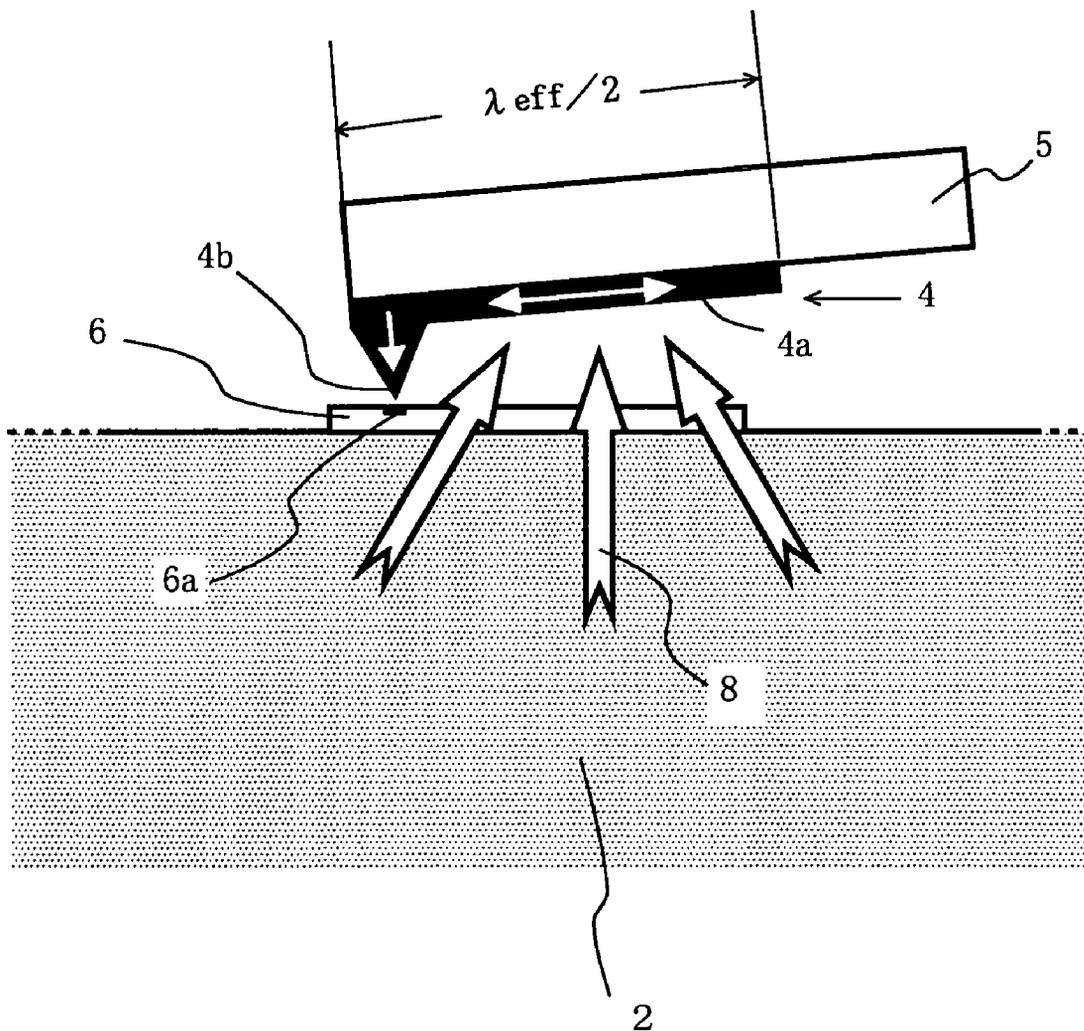


FIG. 3

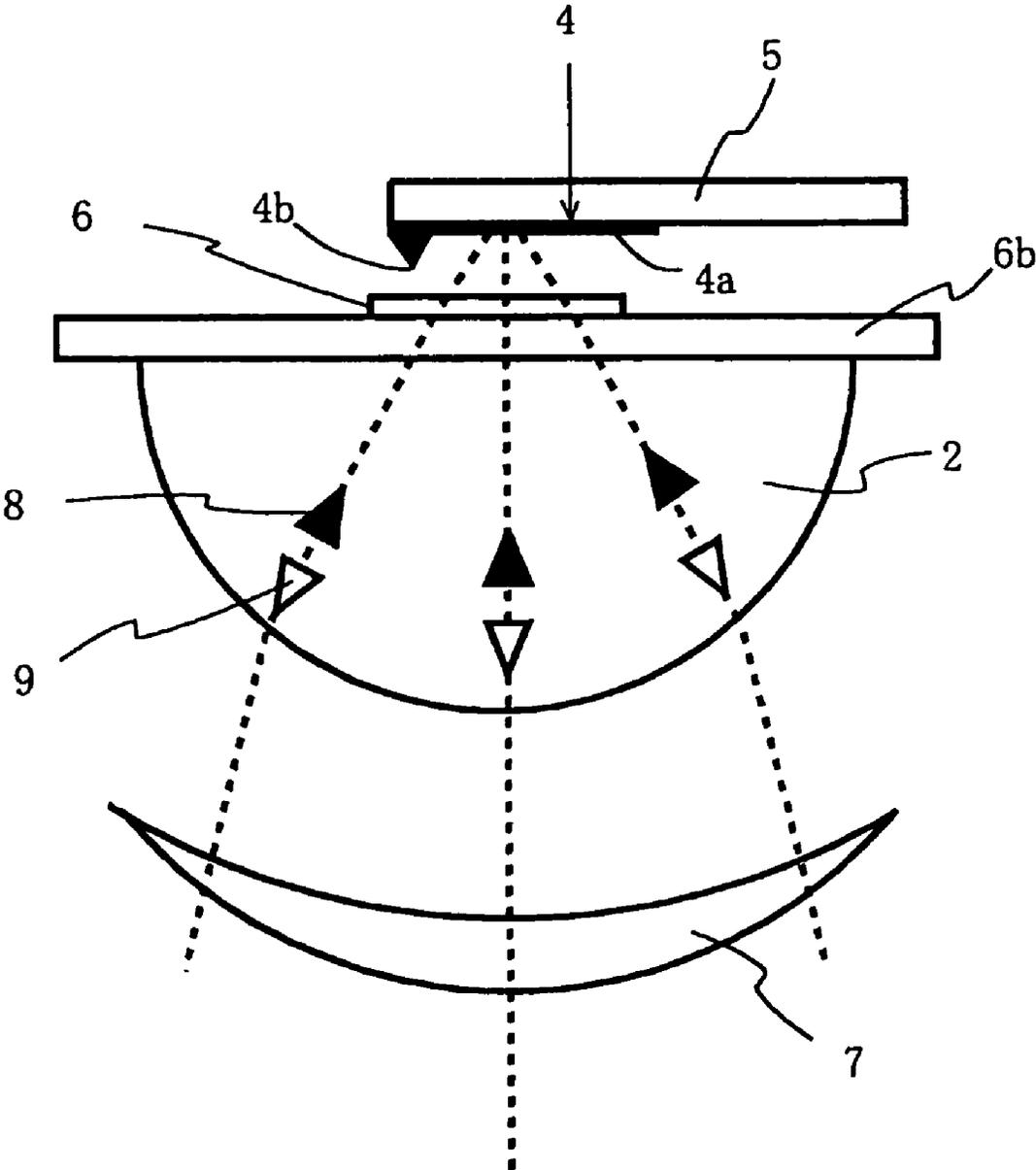


FIG. 4

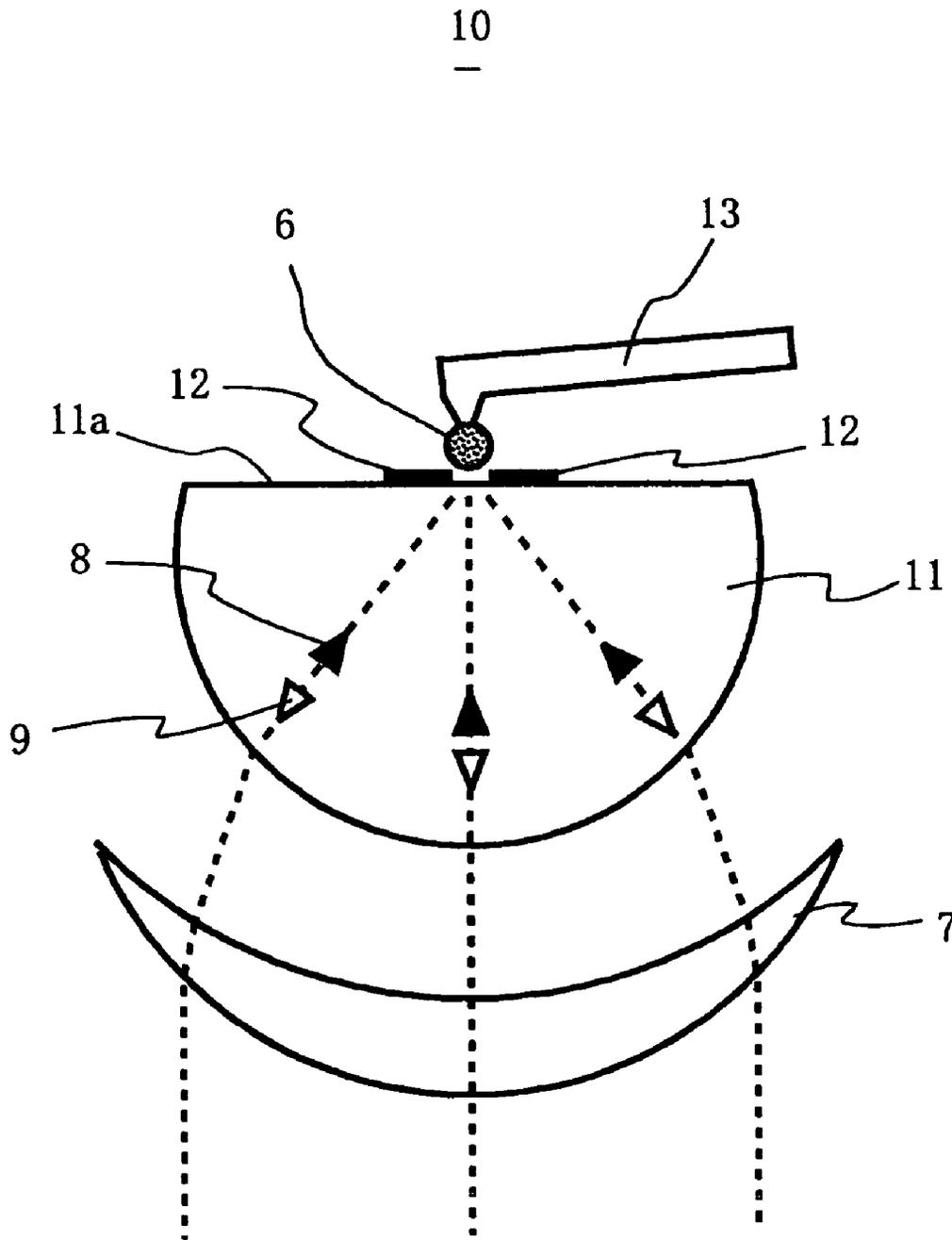


FIG. 5

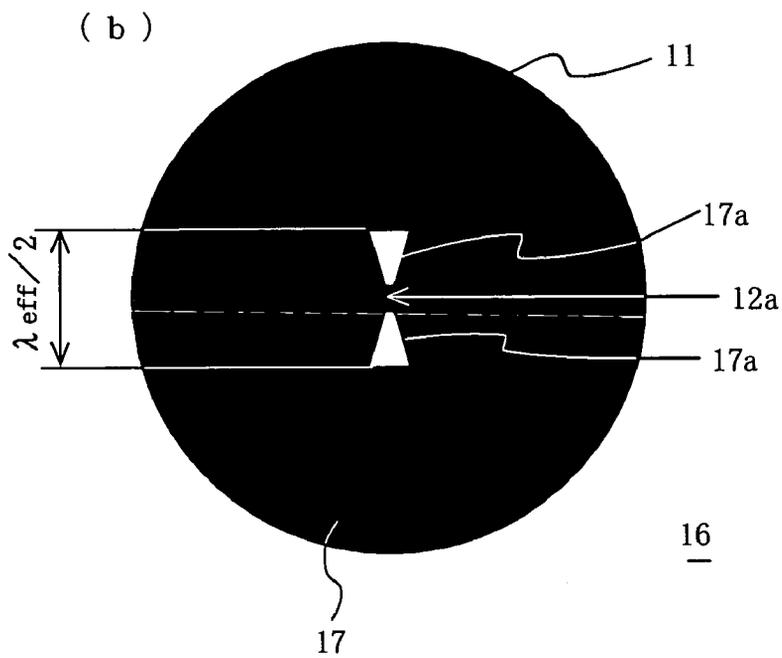
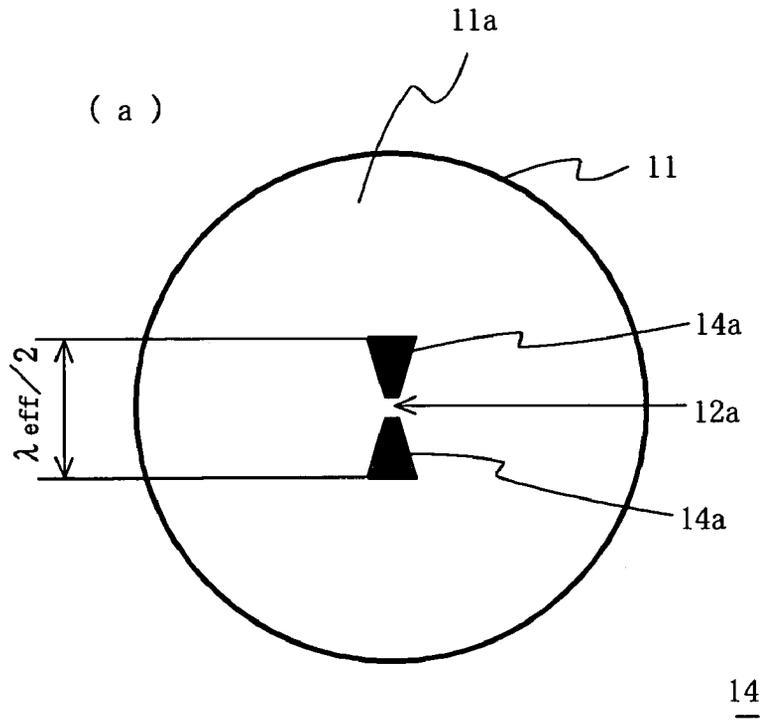


FIG. 6

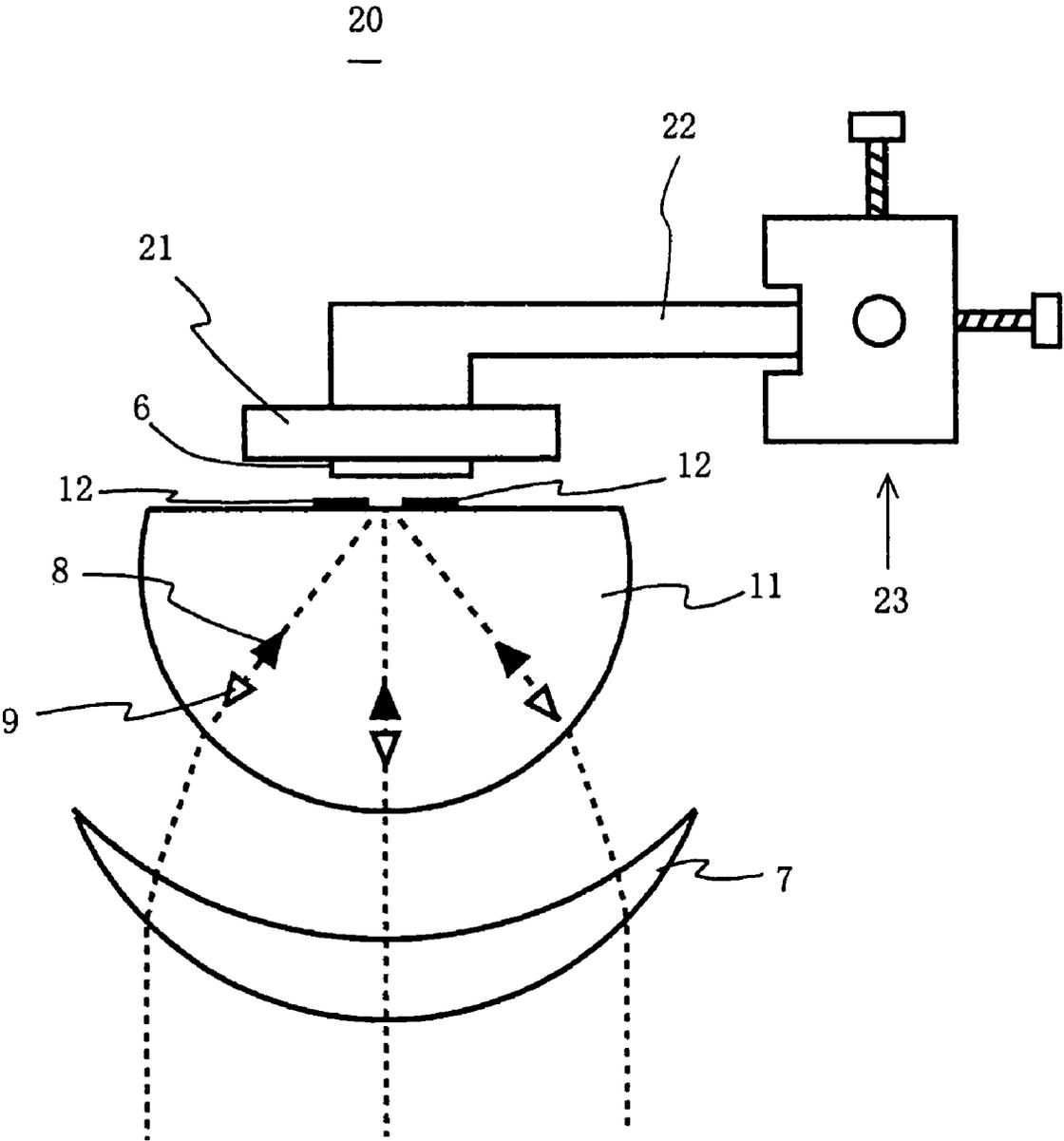
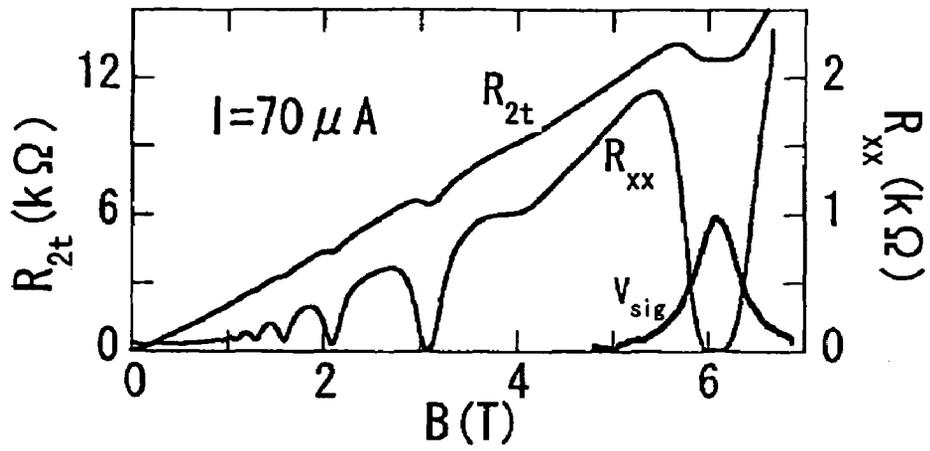


FIG. 7

(a)



(b)

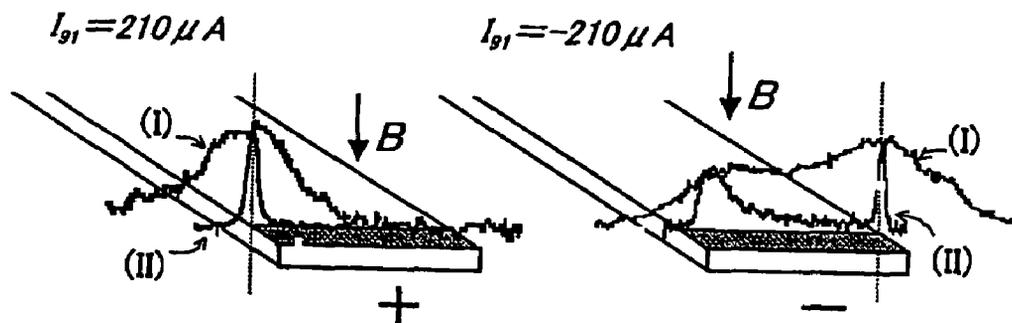


FIG. 8
(Prior Art)

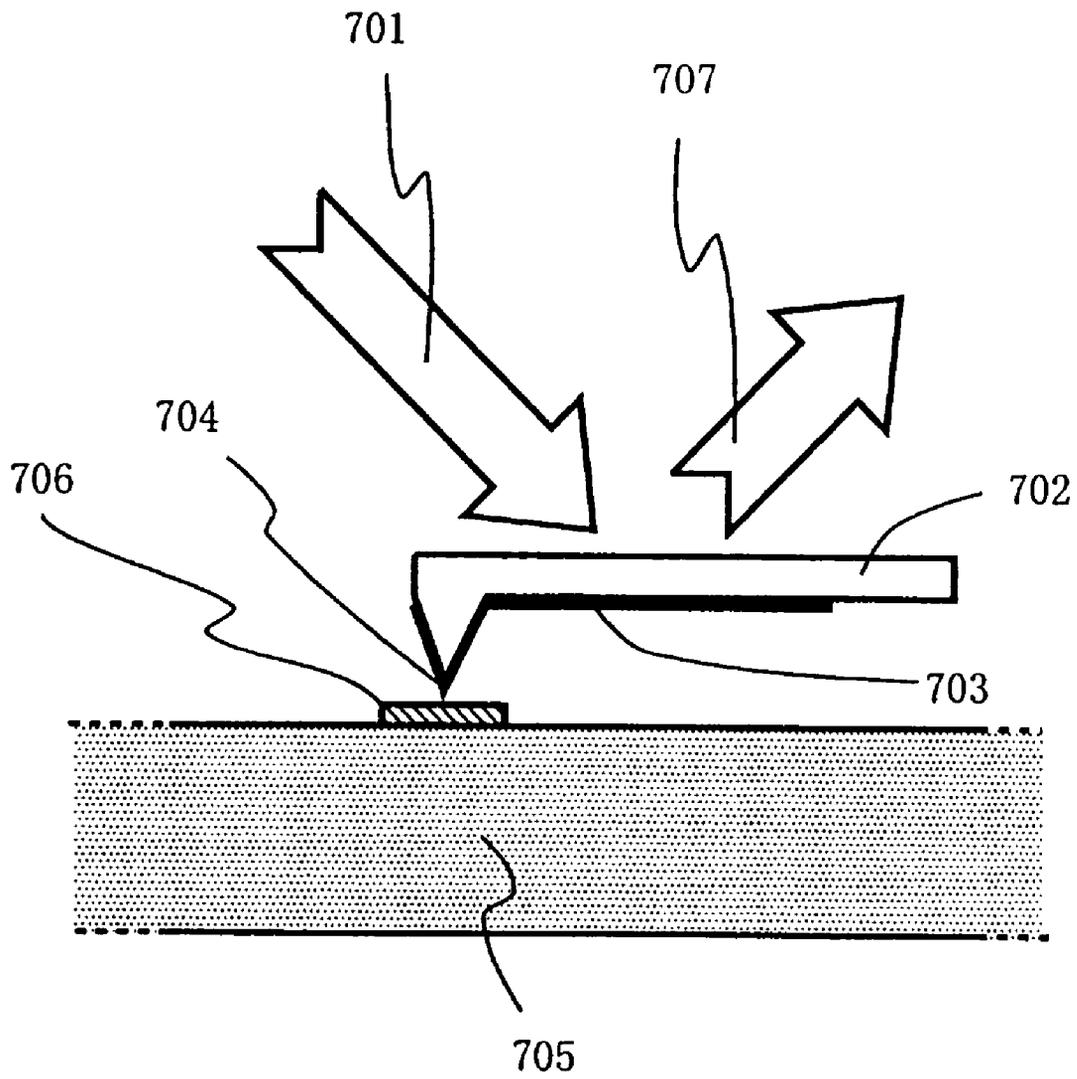


FIG. 9
(Prior Art)

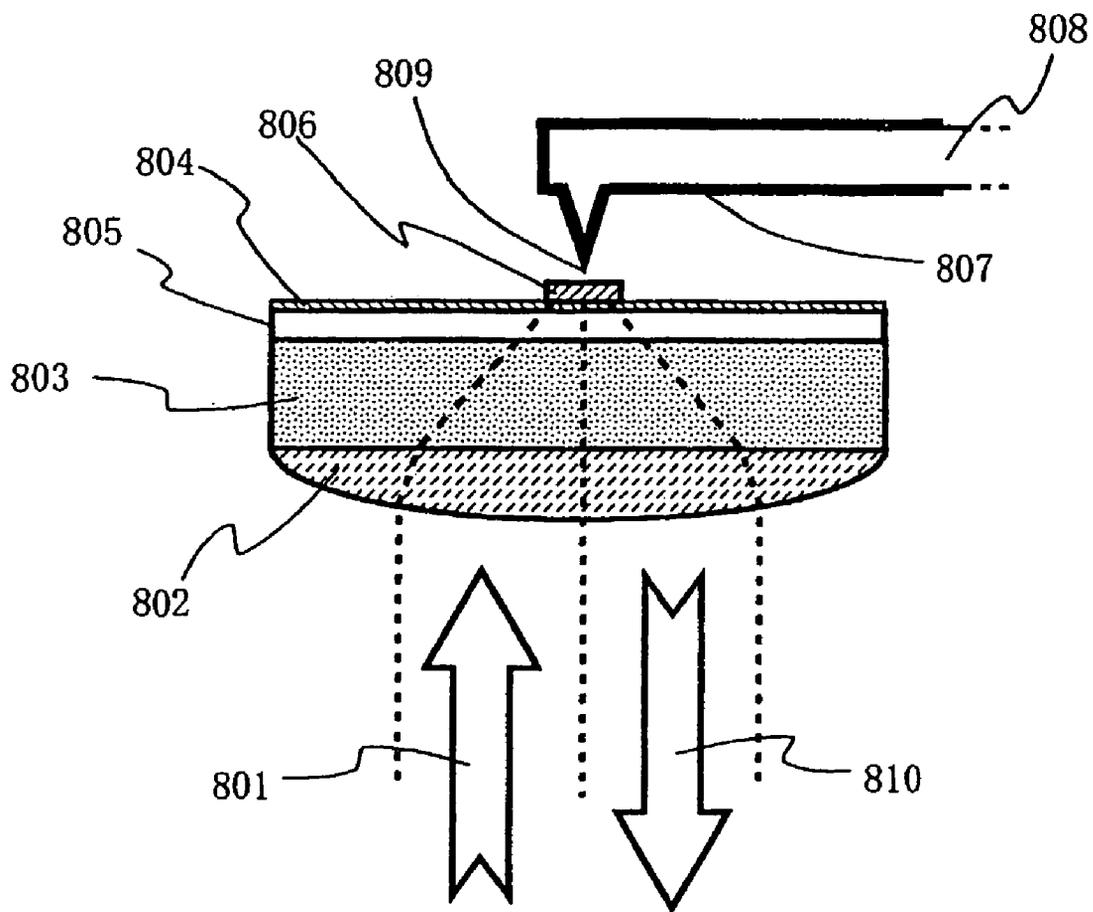
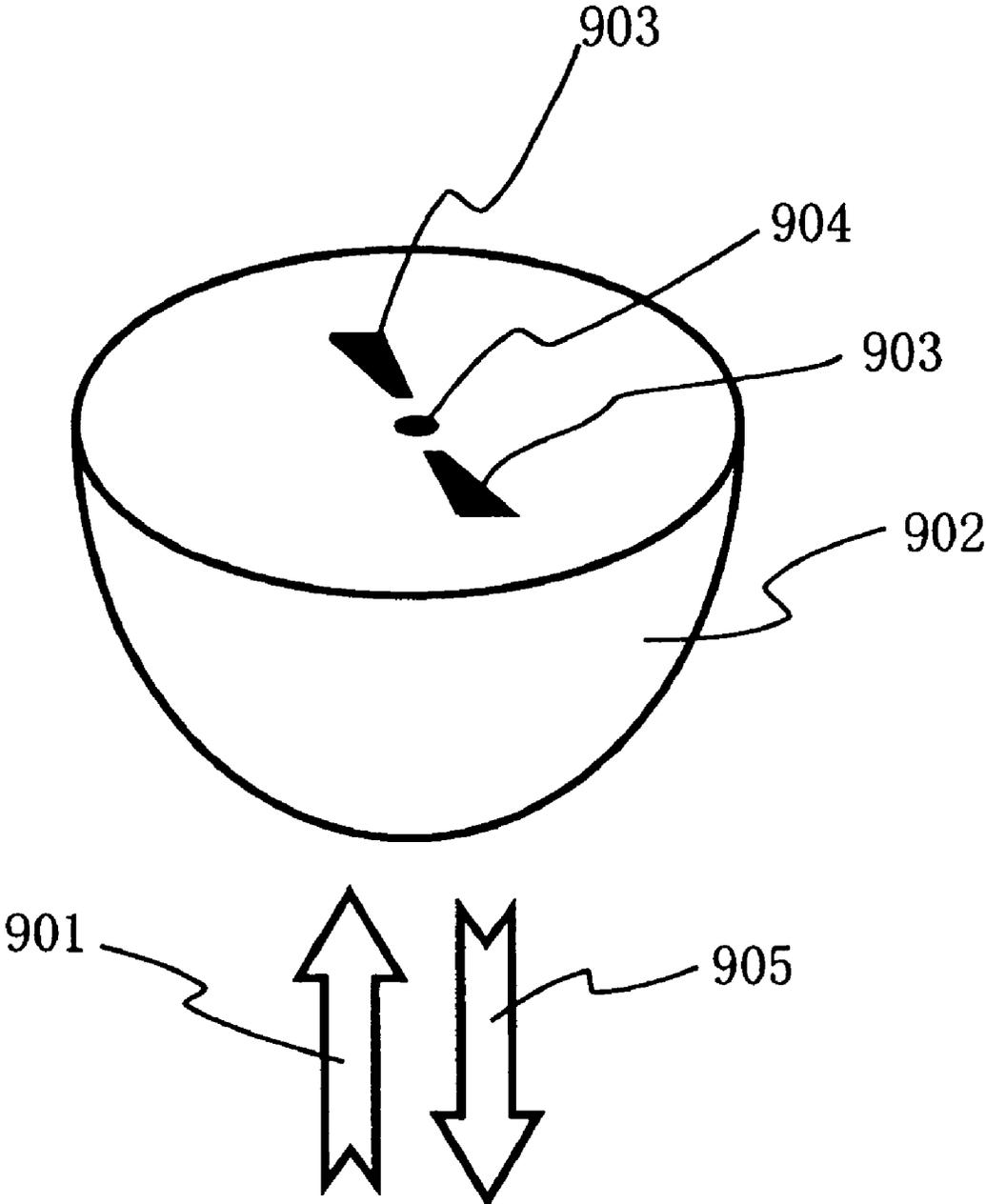


FIG. 10
(Prior Art)



INFRARED FOCUSING DEVICE

TECHNICAL FIELD

The present invention relates to an apparatus for condens-
ing infrared light or microwave into a microfine area or for
collecting infrared light or microwave emitted from a
microfine area, which apparatus is herein referred to as an
“infrared light condensing apparatus”.

BACKGROUND ART

Combining geometrical-optical lenses in any way does not
allow condensing a light into an area as extremely small as
one half of its wavelength because of a diffraction limit of the
light. It is then not possible either to pick up selectively a light
emitted from an area as extremely small as one half of its
wavelength. However, light has not only waves to propagate
as described by the Maxwell's equations but also a near field
that exists only extremely near the surface of an object. If a
probe having a sharply pointed tip whose diameter is as small
as less than the diffraction limit is used to bring this pointed
tip into extremely close proximity to the surface of an object,
there can then be created a near-field coupling between them
to bring about a near field on the object surface, also permit-
ting such a near field from an object to be taken as a light
propagating. Using this method allows an optical image of an
object to be observed at a resolution less than the diffraction
limit and further the nature of matter such as Raman scatter-
ing to be measured at a resolution less than the diffraction
limit.

In the past, however, there has been no technique available
to control positioning a probe having a tip as sharp as less than
the diffraction limit and to control the relationship in position
between the probe tip and a measured object at a resolution
less than the diffraction limit, and for this reason the near-field
could hardly be applied.

In recent years, as represented by the atomic force micro-
scope (AFM) it has become possible to control positioning a
probe whose diameter is on an atomic size level and to control
the relationship in position between the tip of the probe and an
object to be measured three-dimensionally at a resolution less
than an interatomic distance, thus spreading the use of the
near-field applied techniques.

In the near-field applied techniques, however, that utilize
light into and out of an extremely small area and therefore
entail a signal that is extremely small in intensity, obtaining
any information that is meaningful requires that light incident
be condensed into a microfine area very efficiently and that a
near field in such a microfine area be collected very effi-
ciently, and namely calls for a system that is extremely high in
light condensing efficiency. Further, obtaining a near-field
image for a specimen requires that any light condensing posi-
tions be scanned at a resolution less than the diffraction limit.

The conventional near-field application techniques have
the problem that they can scan light condensing positions but
are low in light condensing efficiency or that they are high in
light condensing efficiency but cannot scan light condensing
positions, there being no apparatus which can be put to prac-
tical use by being excellent in light condensing efficiency and
at the same time capable of scanning at a sufficiently high
position resolution. Mention is made below of further details
of the difficulties met by the prior art.

One of the near-field application techniques is a scattering-
type scanning near-field optical microscope abbreviated as
s-SNOM. This is an apparatus that is designed to cause a light
of long wavelength such as a microwave to be condensed into

a microfine area of sub-microns or less in size and an infrared
light or microwave emitted from a microfine area of sub-
microns or less in size to be collected or condensed. It utilizes
a near-field coupling brought about between the sharply
pointed tip of a small electric conductor and an object to be
measured to perform a variety of measurements at a resolu-
tion less than the optical diffraction limit.

FIG. 8 illustrates the operating principles of such a micro-
scope and shows the s-SNOM in a conceptual view as it
condenses an infrared light at an AFM cantilever coated with
an electric conductor. See literature: B. Knoll and F. Keil-
mann, Nature 399 (1999), issued 13 May 1999.

An infrared light **701** is incident from the external free
space on an electric conductor **703** coated on a cantilever **702**,
then concentrating as a near-field at a tip **704** of the electric
conductor **703**. This near-field is coupled with a region, which
is adjacent to the tip **704**, on a specimen **706** mounted on a
specimen support table **705**. And inversely the near-field of
the specimen **706** is coupled with and thereby transmitted to
the tip **704** of the electric conductor **703** which then acting as
an antenna emits it as an infrared light **707** into the external
free space. Here, both the incident and outgoing infrared
lights **701** and **707** are condensed by usual optical lenses (not
shown). According to this apparatus, moving the cantilever
702 to let it scan allows an image by the entire near-field for
the small specimen **706** to be observed at a resolution less
than the diffraction limit.

However, since the proportion at which the infrared light
701 is coupled to the antenna **703** is proportional to factor
(ϵ_0/ϵ_s) where ϵ_0 and ϵ_s are the dielectric constants of the
external space and the specimen support substrate **705**,
respectively, and $\epsilon_0 < \epsilon_s$, the efficiency of the electric con-
ductor **703** as an antenna is rather low. Likewise, the near-
field from the small specimen **706** largely is coupled to the
specimen support substrate **705** high in dielectric constant
and comes to be emitted in its large part into the interior of the
specimen support substrate **705** with only its reduced part
emitted in the form of the infrared light **707**. Thus, this system
has the problem that the efficiency at which to condense an
incident infrared light and the efficiency at which to condense
a near-field from a specimen as an outgoing infrared light,
namely its light condensing efficiency is low.

Another near-field application technique in the prior art is
next shown.

FIG. 9 illustrates a method wherein light is made incident
from the side of a specimen support substrate to obtain Raman
scattering light. See literature: H. Hayazawa et al., Chem.
Phys. Lett. 355 (2001) 369, issued 2 May 2001. An incident
light **801** is condensed by a usual optical lens **802** and then
past a substrate **805** coated with oil **803** and a thin film of
silver **804** is focused on a specimen **806** whereupon a near-
field by the focused light is intensified by surface plasmon
polariton brought about and excited at a tip **809** of a cantilever
808 coated with an electric conductor **807**. And similarly,
Raman scattering light **810** from the specimen **806** intensified
by the surface plasmon polariton brought about and excited at
a tip **809** is taken out and then past the substrate **805** and the
oil **803** is condensed by the lens **802**. According to this
method, scanning the cantilever **808** allows observing a
Raman scattering scanning image of the specimen **806** at a
resolution less than the diffraction limit.

In this method, however, the geometrical size of an electric
conductor **807** as a whole is not taken into consideration,
thereby leaving the electric conductor **807** less functioning as
an antenna. Moreover, its function as an antenna is restricted
by a screening or shielding effect exerted by the silver coating
804 on the specimen support substrate **805**. Thus, lacking an

adequate light focusing capability, the system is low in the efficiency at which to convert the near-field from the small specimen **806** into the outgoing light **810**. To wit, the system has the problem that its light condensing efficiency is low.

By the way, in the field of far-infrared techniques there is known an efficient light condensing method for a microfine absorber in a far-infrared region. FIG. **10** is a conceptual view illustrating such an efficient light condensing method conventionally known for a microfine absorber in a far-infrared region. See literature: "Infrared and Millimeter Waves, Volume 10", Millimeter Components and Techniques, Part II, Chapter 1 (1983), ed. by Academic Press Inc. An incoming light **901** is incident into a solid immersion lens made of dielectric **902** and condensed on a planar dipole antenna or planar slot antenna **903** lying at its focal position. Further, the incident light condensed on the antenna is caused to geometrically resonate by the antenna and focused onto a small far-infrared absorber **904** disposed at the center of the antenna. According to this method in which a far-infrared light is caused to geometrically resonate by an antenna, it is possible to absorb the far-infrared light efficiently and at due sensitivity. Consequently, if a specimen to be measured is disposed in place of the far-infrared absorber **904** at a position at which it is disposed, then it is possible to take out the near-field **905** efficiently.

In this method, however, in which the planar dipole antenna or planar slot antenna **903** is fixed onto the solid immersion lens **902**, it is not possible to move the light focusing position for scanning.

Thus, although there have already been systems designed to condense a light at a microfine area smaller than its diffraction limit or to take up a near-field from a microfine area smaller than its diffraction limit and then to condense it, e.g., to condense an infrared light whose wavelength is several tens microns or more at an area as microfine as sub-microns or less or to take out a near-field from an area as microfine as sub-microns or less and then to condense it, these conventional systems have the problem that they are low in light condensing efficiency or otherwise are incapable of scanning such a microfine position of light condensing, or light taking up.

DISCLOSURE OF THE INVENTION

It is, accordingly, an object of the present invention to provide an infrared light condensing apparatus that is capable of condensing an infrared light whose wavelength is several tens microns or more at an area as microfine as sub-microns or less efficiently and is likewise capable of taking up a near-field from an area as microfine as sub-microns or less and then to condense it and that is at the same time capable of repositioning such an area, thus capable of scanning such a microfine position of light condensing or light taking up

In order to achieve the first object mentioned above there is provided in accordance with the present invention in a first aspect thereof an infrared light condensing apparatus, characterized in that it comprises: a solid immersion lens for accepting an incident light or emitting an outgoing light, the said solid immersion lens having a base plane on which a specimen is to be disposed; an antenna having a probe disposed away from a base plane of the said solid immersion lens at a distance not more than $\frac{1}{4}$ of an effective wavelength of the light; a holder means for retaining the said antenna; and a position control means for controlling the position of a tip of the said probe by means of the said holder means, whereby operating the said position control means allows:

the incident light to concentrate as a near-field at a desired position of the specimen on the base plane of the said solid immersion or

a near-field from a desired position of the specimen to be converted into a propagating wave corresponding thereto and then the propagating wave to be emitted as the said outgoing light from the said solid immersion lens.

Specifically, the said solid immersion lens is composed of a medium that is low in absorption coefficient and large in dielectric constant for wavelengths of the said incident or outgoing light, while the distance between the said antenna and the base plane of the said solid immersion lens is less than $\frac{1}{4}$ of the effective wavelength of the light. This is to cause an incident light propagating in a medium of high dielectric constant to be efficiently coupled to an antenna and to cause an outgoing light to be emitted from an antenna into a medium of high dielectric constant, both of which characterizes an antenna enhanced in efficiency.

To wit, coupling of an incident or an outgoing light to an antenna in a medium of high dielectric constant is made better in efficiency than in a free space (vacuum or air) by a factor of $(\epsilon_s/\epsilon_o)^{3/2}$ where ϵ_s and ϵ_o are dielectric constants of the medium and free space, respectively. See literature: "Infrared and Millimeter Waves, Volume 10", Millimeter Components and Techniques, Part II, Chapter 1 (1983), ed. by Academic Press Inc. For example, when the solid immersion lens is composed of silicon ($\epsilon_s=12.8 \epsilon_o$), gallium ($\epsilon_s=12.5 \epsilon_o$), germanium ($\epsilon_s=16 \epsilon_o$) or the like, the improvement in efficiency reaches several tens times over in the free space.

Thus, a first feature of the present invention lies in coupling an incident or outgoing light to an antenna in a medium of high dielectric constant to enhance the light condensing efficiency of the antenna.

Also, the said antenna mentioned above may specifically be made of an electric conductor having a length that is half the effective wavelength of the incident or outgoing light to bring the incident or outgoing light into geometrical resonance with the antenna. Then, the incident light can be condensed and the outgoing light can be emitted, both extremely efficiently. Here, the term "effective wavelength" refers to a wavelength defined by $\lambda_{eff}=\lambda/[\epsilon_o+\epsilon_s]^{1/2}$ where ϵ_o is dielectric constant of vacuum, ϵ_s is dielectric constant of the solid immersion lens and λ is vacuum wavelength. Further, the said probe specifically may have its tip that is a sharply pointed edge of a rod-like electric conductor having a radius of curvature less than a diffraction limit of the incident or outgoing light and may be configured to project from the said electric conductor towards the specimen. Then, it is made possible to concentrate a near-field in a microfine area less than the light diffraction limit on the specimen and also to probe and pick up a near-field in a microfine area less than the light diffraction limit on the specimen. Thus, it is a second feature of the present invention to use an antenna that brings about geometrical resonance to enhance the light condensing efficiency of an incident or outgoing light.

Also, specifically the said holder means may comprise an arm and said position control means may comprise a triaxial XYZ mechanical stage. This permits the triaxial XYZ mechanical stage to be operated with the arm to three-dimensionally control the relationship in position between the probe tip and the specimen surface at a resolution less than the diffraction limit of the incident or outgoing light.

Also, specifically the said holder means may alternatively comprise a cantilever having a rear face reflecting an incident laser light and the said position control means may then be responsive to a change in angle of reflection of the laser light

at the cantilever rear face in an arrangement as well known with the conventional AFM or the like, thereby permitting the relationship in position between the probe tip and the specimen surface to be controlled three-dimensionally at a further enhanced resolution less than the diffraction limit of the incident or outgoing light.

Also, if the position control means is operated to move the specimen for its scanning over a distance within a range of one half of the effective wavelength, there can in no case be the focal point of the solid immersion lens dislocated out of the antenna. It is therefore possible to convert an incident light into a near-field and then to concentrate it at a desired position or to convert a near-field at a desired position to an outgoing light and then to take out it, without lowering the due light condensing efficiency. It is therefore a third feature of the present invention to make it possible to scan a specimen while maintaining the light condensing efficiency high.

The present invention provides in a second aspect thereof an infrared light condensing apparatus characterized in that it comprises: a solid immersion lens for accepting an incident light or emitting an outgoing light; an antenna disposed on a base plane of the said solid immersion lens; a holder means for retaining a specimen adjacent to the said antenna; a position control means for controlling the position of the said holder means, whereby operating the said position control means allows:

the incident light to concentrate as a near-field at a desired position of the specimen retained by the said holder means or

a near-field from a desired position of the specimen to be converted into a propagating wave corresponding thereto and then the propagating wave to be emitted as the said outgoing light from the said solid immersion lens.

The solid immersion lens may here again be composed of a medium that is low in absorption coefficient and large in dielectric constant for wavelengths of the incident or outgoing light, thereby permitting the incident or outgoing light to be coupled to the antenna in the medium of high dielectric constant to enhance its light condensing efficiency.

Also, specifically the said antenna may be a planar dipole antenna or a planar slot antenna disposed on a base plane of the said solid immersion lens in a region of its focal position. The said planar dipole antenna may be a bowtie antenna made of a pair of generally triangular electric conductors whose apexes are opposed to each other at a small distance less than a diffraction limit of the incident or outgoing light, the bowtie antenna having a total length that is one half of an effective wavelength of the incident or outgoing light. The said planar slot antenna may be a bowtie antenna made of an electric conductor having a pair of generally triangular windows formed therein whose apexes are opposed to each other at a small distance less than a diffraction limit of the incident or outgoing light, the bowtie antenna having a total length that is one half of an effective wavelength of the incident or outgoing light.

According to this makeup, an incident light is allowed to geometrically resonate with a planar dipole or slot antenna to generate a near-field and can be concentrated at a microfine area on a specimen efficiently. Alternatively, it is made possible to convert a near-field from a specimen into a propagating wave and take it out efficiently. Further, adjusting the essentially triangular configuration allows impedance-matching to further enhance the efficiency.

Also, specifically the said holder means may comprise an arm and said position control means may comprise a triaxial XYZ mechanical stage. This permits the triaxial XYZ

mechanical stage to be operated with the arm to three-dimensionally control the relationship in position between the probe tip and the specimen surface at a resolution less than the diffraction limit of the incident or outgoing light.

Also, specifically the said holder means may alternatively comprise a cantilever having a rear face reflecting an incident laser light and the said position control means may then be responsive to a change in angle of reflection of the laser light at the cantilever rear face in an arrangement as well known with the conventional AFM or the like, thereby permitting the relationship in position between the probe tip and the specimen surface to be controlled three-dimensionally at a further enhanced resolution less than the diffraction limit of the incident or outgoing light.

Operating the position control means in this way to cause a desired position of a specimen retained by a holder means to be brought proximal to a focal position of a planar dipole or slot antenna allows concentrating an incident light as a near-field at the desired position of the specimen or picking up a near-field at the desired position of the specimen and converting it into a propagating wave to emit the latter as an outgoing light into the solid immersion lens medium.

The infrared light condensing apparatus according to the second aspect of the present invention is designed to move the specimen to obtain its scanning image while the infrared light condensing apparatus according to the first aspect of the invention is designed to move the antenna to scan the specimen for obtaining its scanning image.

While the first infrared light condensing apparatus of the invention has its resolution determined by the curvature of the probe tip, the apparatus according to the second aspect of the invention has the feature that its resolution is determined by a microfine area positioned at the center of the bowtie antenna, whose shape and surface area and any other geometric parameter can readily be varied by a particular design of the bowtie antenna. The bowtie antenna, which can be readily made up, e.g., by forming a pattern metal film on the base plane of a solid immersion lens, makes it possible to build up an apparatus with a resolution optimal to a particular specimen to be measured and a particular purpose of measurement.

BRIEF DESCRIPTION OF THE DRAWINGS

The present invention will better be understood from the following detailed description and the drawings attached hereto showing certain illustrative forms of implementation of the present invention. In this connection, it should be noted that such forms of implementation illustrated in the accompanying drawings hereof are intended in no way to limit the present invention but to facilitate an explanation and understanding thereof. In the drawings,

FIG. 1 is a schematic view illustrating an infrared light condensing apparatus that represents a first form of implementation of the present invention;

FIG. 2 is an enlarged view of an essential part of the apparatus shown in FIG. 1 for illustrating an operation thereof;

FIG. 3 is a schematic view illustrating a modification of the apparatus of FIG. 1;

FIG. 4 is a schematic view illustrating an infrared light condensing apparatus that represents a second form of implementation of the present invention;

FIG. 5 shows at (a) and (b) the constructions of a planar dipole antenna and a planar slot antenna, respectively, that can be formed on a base plane of a solid immersion lens;

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FIG. 6 is a schematic view illustrating an infrared light condensing apparatus that represents a third form of implementation of the present invention;

FIG. 7 shows results of measurement of an edge current based on the quantum Hall effect according to an apparatus of the present invention wherein (a) is a graph illustrating the quantum Hall effect for a measured specimen and (b) shows distributions of the measured edge current;

FIG. 8 is a makeup diagram of a near-field light condensing apparatus according to the prior art;

FIG. 9 is a makeup diagram of a conventional light condensing apparatus for use in Raman scattering; and

FIG. 10 is a makeup diagram of a conventional light condensing apparatus for use in a far-infrared absorber.

BEST MODES FOR CARRYING OUT THE INVENTION

Hereinafter, the present invention will be described in detail with reference to forms of implementation thereof illustrated in the drawing figures.

FIG. 1 is a diagram illustrating an infrared light condensing apparatus according to a first form of implementation of the present invention, and FIG. 2 is an enlarged view of an essential part of the apparatus shown in FIG. 1 for illustrating an operation thereof. The apparatus of the invention indicated by reference character 1 comprises a solid immersion lens 2, an antenna 4 spaced apart at a distance from a base plane 3 of the solid immersion lens 3, a cantilever 5 that holds the antenna 4 thereon, and a position control unit (not shown) for controlling the position of the cantilever 5. The antenna 4 as shown enlarged in FIG. 2 is made of an electric conductor 4a having a length that is one half of an effective wavelength λ_{eff} of a light and a probe 4b projecting from the electric conductor 4a towards the base plane 3. Here, the effective wavelength λ_{eff} is a wavelength defined by $\lambda_{eff} = \lambda / [\epsilon_o + \epsilon_s]^{1/2}$ where ϵ_o is dielectric constant of vacuum, ϵ_s is dielectric constant of the solid immersion lens and λ is vacuum wavelength. On the other hand, the probe 4b is either itself electrically conductive or coated on its surface with an electric conductor and is made electrically integral with the electric conductor 4a. The probe 4b is here a rod-like electric conductor having a sharply pointed edge with its radius of curvature as small as submicron or less. Each part of the antenna 4 is disposed away from the base plane 3 of the solid immersion lens 2 at a distance within $\lambda_{eff}/4$. A specimen 6 to be measured is disposed on the base plane 3 of the solid immersion lens 2 in a region of its center.

The cantilever 5 is controlled in position by a conventional control means as well known, e.g., with the AFM. For example, if an amount of bending of the cantilever 5 due to an atomic force between surface atoms of the tip of the probe 4b and the specimen 6 is taken as an angle of reflection by a rear surface of the cantilever 5 of a laser light impinging thereon, and the amount of bending is maintained constant by adjusting the height so as to be the angle constant, it is then possible to control and maintain the distance between the tip of the probe 4b and the specimen 6 at an accuracy within 0.1 nm. Also, high-precision positioning control in planar directions can be achieved using a piezoelectric stage.

Mention is next made of an operation of the apparatus illustrated. Referring to FIG. 1, an infrared light 8 incident from below via a usual optical lens 7 into the solid immersion lens 2 is past a specimen 6 mounted on its base plane 3 and is focused on the antenna 4 where it is converted into a high-frequency electric current. Then, the spacing between the antenna 4 and the base plane 3 is so small that the dielectric

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constant which the infrared light feels is dielectric constant ϵ_s of the solid immersion lens 2. And then, high dielectric constant ϵ_s of the medium from which the infrared light 8 is incident into the antenna 4 increases the electromagnetic power of the infrared light 8, i.e., induces a large electromagnetic current in the antenna 4. To wit, coupling of an incident infrared light to an antenna in such a medium is made better in efficiency than in a free space (vacuum or air) by a factor of $(\epsilon_s/\epsilon_o)^{3/2}$ where ϵ_s and ϵ_o are dielectric constants of the medium and free space, respectively. For example, when the solid immersion lens and the specimen support table are composed of silicon ($\epsilon_s=12.8 \epsilon_o$), gallium ($\epsilon_s=12.5 \epsilon_o$), germanium ($\epsilon_s=16 \epsilon_o$) or the like, the improvement in efficiency reaches several tens times over in the free space.

Also, where as shown in FIG. 2 the antenna 4 has a length that is one half of its effective wavelength there, the infrared light 8 is brought into geometrical resonance and coupled to the antenna 4 at an enhanced efficiency. As a result, the infrared light as indicated by the white arrows in the Figure induces a high-frequency electric current in the electric conductor 4a efficiently and the high-frequency electric current in turn forms a strong near-field localized at a portion 6a of the specimen that is adjacent to the tip apex of the probe 4b. Thus, the apparatus according to the present invention is capable of focusing or concentrating an incident infrared light 8 efficiently at a submicron area 6a of the specimen, thanks to two-step concentrating actions, namely by the high-dielectric-constant solid immersion lens focusing it at the antenna 4 and by the geometric resonance with the antenna 4 concentrating the near-field at the tip apex of the probe 4b. A light from the submicron area 6a can likewise be picked up efficiently. To wit, if a microfine area 6a of the specimen emits or scatters an infrared light 9, then the infrared light 9 can be picked up with the intermediary of its near-field coupling to the tip apex 4b and led with the intermediary of its geometric resonance in the antenna 4 into the high dielectric constant solid immersion lens 2, thereby permitting the infrared light 9 to be taken out as an outgoing light into the outside efficiently. Moreover, with the antenna 4 having its length one half of the effective wavelength λ_{eff} of the light, moving to position the cantilever 5 within this length range does not affect the light condensing efficiency, permitting a scanning image over a length that is one half of the effective wavelength λ_{eff} to be obtained. Also, scanning using a position control means as used in the AFM or the like allows a scanning image to be obtained at an extremely high resolution.

FIG. 3 is a diagram illustrating the makeup of a modification of the first form of implementation of the present invention. Compared with the apparatus shown in FIG. 1, it differs in that there is provided a specimen support table 6b that supports or retains a specimen 6 thereon. The specimen support table 6b is composed of a material which is preferably identical to that of which the solid immersion lens 2 is composed but which if not identical should desirably be less in pick-up capability for wavelengths of the incident light or the outgoing light 9 and high in dielectric constant. In this modified apparatus, it is also important to adjust the solid immersion lens 2 and the specimen support table 6b in thickness so that the infrared light 8 past the solid immersion lens 2 and the specimen support table 6b is focused on the antenna conductor 4a.

An explanation is next given in respect of a second form of implementation of the present invention.

FIG. 4 is a diagram illustrating an infrared light condensing apparatus according to the second form of implementation of the present invention. This apparatus indicated by reference character 10 comprises a solid immersion lens 11, an antenna

12 formed on a base plane **11a** of the solid immersion lens **11**, a cantilever **13** disposed adjacent to the antenna **12** to carry a specimen, and a position control means (not shown) for controlling the position of the cantilever **13**.

FIG. **5** shows at (a) and (b) the constructions of a planar dipole antenna **14** and a planar slot antenna **16**, respectively, each of which is shown formed on the base plane **11a** of the solid immersion lens **11**. The planar dipole antenna **14** and the planar slot antenna **16** are each formed in the form of electrically conductive thin film at a focal position on the base plane **11a** of the solid immersion lens **11**. The planar dipole antenna **14** as shown in FIG. **5(a)** is a bowtie antenna which is made of a pair of generally triangular electric conductors **14a** whose apexes are opposed to each other across a small spacing **12a** less than the diffraction limit of an incident or outgoing light, the bowtie antenna having a total length that is one half of an effective wavelength λ_{eff} of the incident or outgoing light. The planar slot antenna **16** as shown in FIG. **5(b)** is a bowtie antenna which is made of an electric conductor **17** in which are formed a pair of generally triangular windows **17a** and **17b** whose apexes are opposed to each other across a small spacing **12a** less than the diffraction limit of an incident or outgoing light, the bowtie antenna having a total length that is one half of an effective wavelength λ_{eff} of the incident or outgoing light.

Mention is next made of an operation of the apparatus.

Referring to FIG. **4**, an infrared light incident from below via a usual optical lens **7** into the solid immersion lens **11** is condensed at the antenna **12** by the usual geometrical-optical light condensing action of the solid immersion lens. In the antenna **12** it is then converted into a high-frequency electric current while causing a near-field to develop and concentrate at a microfine area **12a** in the antenna **12**. And then, as in the first apparatus mentioned above, high dielectric constant ϵ_s of the medium from which the infrared light **8** is incident into the antenna **12** increases the electromagnetic power of the infrared light **8**, i.g., induces a large electromagnetic current in the antenna **12**.

Also, with the bowtie antenna **14**, **16** having its total length one half of the effective wavelength λ_{eff} as shown in FIG. **5**, the condensed infrared light **8** is caused to geometrically resonate therewith, thereby concentrating the near-field (electric-field component) of the infrared light **8** at the microfine area **12a** efficiently. The near-field formed localized efficiently at the microfine area **12a** in the antenna **12** forms a near-field at a portion of the specimen **6** that is immediately adjacent thereto. The specimen **6** mounted on the cantilever **13** is moved controllably by the position control means as in the first apparatus mentioned above to successively change its position at which the near-field is created, thereby permitting its scanning.

The resolution in this apparatus is determined by the size of the microfine area **12a** located at the center of the bowtie antenna **14**, **16**. The microfine area **12a** can be varied in size in terms of its one side length from 10 microns to 0.05 micron depending on a particular wavelength of the infrared light and a particular space resolution required in measurement. The bowtie antenna, which can be readily made up, e.g., by forming a pattern metal film on the base plane of a solid immersion lens, makes it possible to build up an apparatus with a resolution optimal to a particular specimen to be measured and a particular purpose of measurement.

Likewise, a near-field from a microfine area **12a** can also be taken out efficiently in the form of a propagating wave. To wit, if a portion of the specimen **6** that is immediately adjacent to the microfine area **12a** emits or scatters an infrared light **9**, then an oscillating current is induced in the bowtie antenna

14, **16** with the intermediary of its near-field coupling to the microfine area **12a** and is caused to geometrically resonate with the bow-tie antenna **14**, **16** to allow the infrared light **9** to be emitted in the form of a propagating wave into the solid immersion lens **1** made up of the high dielectric constant medium and the emitted infrared light **9** to be taken out of the solid immersion lens **11** efficiently into the outside. Also, position control using the cantilever **13** allows obtaining a scan image at a resolution of submicron.

It should be noted here that the planar dipole antenna and the planar slot antenna shown in FIG. **5(a)** and FIG. **5(b)** may be modified in a variety of ways depending on the nature and shape of a specimen to be measured. It is only essential that the size of the required near-field area be definitely established and that according to the size established the antenna be designed so that its geometry be adequate to cause an incident light to create geometrical resonance with the antenna and their impedance matching conditions are met. These requirements in conjunction with the known theory relating to an antenna on a medium allows an antenna of this type to be designed optimally according to a particular specimen to be actually measured in practice and a particular wavelength of the infrared light used. See literature: "Infrared and Millimeter Waves, Volume 10", Millimeter Components and Techniques, Part II, Chapter 1 (1983), ed. by Academic Press Inc.

An explanation is next given in respect of a third form of implementation of the present invention.

FIG. **6** is a diagram illustrating an infrared light condensing apparatus according to the third form of implementation of the present invention. This third apparatus, designated by reference character **20**, of the invention is identical in make up to the apparatus **10** in FIG. **4** except that the cantilever **13** used to retain a specimen is replaced with a specimen support **21** for supporting a specimen and an arm **22** for supporting the specimen support **21** and the position control means for controlling the position of the arm **22** comprises a triaxial XYZ precision mechanical stage **23**. Alternatively, it is possible, though not shown, to replace the cantilever **5** for supporting the antenna **4** in the apparatus shown in FIG. **1** with an arm and to use a triaxial XYZ precision mechanical stage for controlling the position of this arm.

Mention is next made of a specific example of the present invention.

This specific example used an apparatus constructed as shown in FIG. **6**. The apparatus was made using a solid immersion lens composed of silicon crystal. The solid immersion lens had a radius of curvature of 1.4 mm and a thickness in its center axis of 1.98 mm. FIG. **7** shows results of measurement based on the quantum Hall effect according to an apparatus of the present invention wherein (a) is a graph illustrating the quantum Hall effect for a measured specimen and (b) shows distributions of the measured far-infrared light. The measured specimen is a two-dimensional electron system in a substrate of aluminum-gallium-arsenic/gallium-arsenic heterostructure. The substrate had a thickness of 0.5 mm and the two-dimensional electron system existed at a depth of 0.1 micron from the substrate surface. The specimen was prepared as a Hall bar device of 4 mm long and 1.5 mm wide retaining the two-dimensional electron system. The Hall bar specimen exhibited the quantum Hall effect under a strong magnetic field at a liquid helium temperature as indicated by the graph for resistances in FIG. **7(a)**.

The Hall bar specimen retained on the substrate was held by the arm **22** in the triaxial XYZ precision mechanical stage **23**. While the specimen was being swept along the surface of the solid immersion lens, the intensity distribution of

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extremely weak far-infrared light emissions from the specimen successively from its edge was picked up. The results of measurement are shown in FIG. 7(b). The measurement was made in a magnetic field of about 6 T and the far-infrared light had a vacuum wavelength of 125 μm . In the graphs of FIG. 7(b) the curves (II) represent results of measurement according to the apparatus of the present invention whereas the curves (I) represent results of measurement according to the prior art method.

Comparison of the results of measurement according to the present invention with those according to the prior art indicates, first, that an improvement by a factor 20 is obtained in the intensity of far-infrared light observed by the present invention over the prior art (note, however, that in FIG. 7(b) the light intensity maximum values of both cases are shown to apparently coincide in order to show a difference between them in spatial resolution to be identified below). Secondly, it is indicated as is apparent from comparison of (I) and (II) in FIG. 7(b) that the spatial resolution is improved remarkably from about 0.5 mm to about 0.06 mm.

According to an apparatus of the present invention in which a light is condensed through a solid immersion lens made of a medium that is high in dielectric constant and a near-field is taken out via such a solid immersion lens, it is seen that marked improvements in both sensitivity and resolution are attained over the prior art. In the specific example above, however, the solid immersion lens had not an antenna formed on its surface and for this reason, a resolution of submicron is not shown. However, the effect achieved when an antenna is formed on such a surface should be apparent from specific examples of the conventional pick-up. See literature: "Infrared and Millimeter Waves, Volume 10", Millimeter Components and Techniques, Part II, Chapter 1 (1983), ed. by Academic Press Inc.

INDUSTRIAL APPLICABILITY

As will be appreciated from the foregoing description, the present invention designed to cause an infrared light to be condensed via a medium of high index of refraction and upon being excited into geometrical resonance makes it possible for an infrared light of several tens micros or more in wavelength to be focused as a near-field at a very small area of submicron or less at an extremely enhanced efficiency and also for a near-field from a very small area of submicron or less to be taken out at a high efficiency. Further, given the positioning control capability with a cantilever at high precision, the present invention makes it possible to obtain a scanning image at a resolution within submicron.

Accordingly, without necessitating an incident light source particularly high in intensity, it is made possible to provide an optical instrument, such as an infrared microscope, a far-infrared microscope, a microwave microscope, a Raman spectrographic microscope and an infrared fluorescence microscope, having a resolution limit less than the diffraction limit of a light used and at the same time permitting a scanning image to be obtained.

The invention claimed is:

1. An infrared light condensing apparatus, comprising:

a solid immersion lens for accepting an incident light or emitting an outgoing light, said solid immersion lens having a base plane on which a specimen is disposed in direct contact with the solid immersion lens;

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an antenna comprising an electrically conductive material, the antenna having a probe disposed away from said base plane of said solid immersion lens at a distance not more than $\frac{1}{4}$ of an effective wavelength of the light;

a holder means for retaining said antenna; and

a position control means for controlling a position of a tip of said probe by means of said holder means,

wherein operating said position control means allows:

the incident light to concentrate as a near-field at a desired position of the specimen on the base plane of said solid immersion lens or

a near-field from a desired position of the specimen to be converted into a propagating wave corresponding thereto and then the propagating wave to be emitted as said outgoing light from said solid immersion lens.

2. An infrared light condensing apparatus as set forth in claim 1, wherein said solid immersion lens comprises a medium that is low in absorption coefficient and large in dielectric constant for wavelengths of said incident or outgoing light.

3. An infrared light condensing apparatus as set forth in claim 1 or 2, wherein said antenna comprises an electric conductor having a length that is one half of the effective wavelength of said incident or outgoing light

to condense the incident light upon causing it to geometrically resonate or

to pick up a near-field from said specimen in a region of the pointed tip of said probe upon causing it to geometrically resonate and then to emit it as a wave propagating in the medium of said solid immersion lens.

4. An infrared light condensing apparatus as set forth in claim 1 or 2, wherein the tip of said probe is a sharply pointed end of a rod-like electric conductor having a radius of curvature less than a diffraction limit of said incident or outgoing light and is configured to project from said electric conductor towards said specimen

to cause the geometrically resonating incident light condensed on said antenna to concentrate as a near-field at said probe tip or

to take out a near-field from a surface of said specimen.

5. An infrared light condensing apparatus as set forth in claim 1 or 2, wherein said holder means comprises an arm and said position control means comprises a triaxial XYZ mechanical stage.

6. An infrared light condensing apparatus as set forth in claim 1 or 2, wherein said holder means comprises a cantilever having a rear face reflecting an incident laser light and said position control means is adapted to respond to a change in angle of reflection of the laser light at the cantilever rear face for controlling the distance between said probe tip and the surface of said specimen.

7. An infrared light condensing apparatus as set forth in claim 1, wherein said holder means is a cantilever.

8. An infrared light condensing apparatus as set forth in claim 7, wherein said cantilever is scanned by said position control means.

9. An infrared light condensing apparatus as set forth in claim 7, wherein said position control means controls the distance between said probe tip and the surface of said specimen, responding to a change in angle of reflection of the laser light at the rear face of said cantilever.

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